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TITLE

Fatigue Crack Initiation and Growth in A517 SAW Weldments Under Variable Amplitude Loading

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# Fatigue Crack Initiation and Growth in A517 SAW Weldments Under Variable Amplitude Loading

by Christopher Bayley<sup>1</sup> and John Porter<sup>2</sup>

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## ABSTRACT

A comparison between experimental and analytical predicted fatigue lives is made for a A517 SAW Weldment subjected to variable amplitude loading. Three, 10 inch wide butt-welded specimens were tested under a variable amplitude load spectrum consisting of 3 yearly storms. The magnitude of the loads in the storm increased and then decreased in a linear manner with the winter storm representing the most severe loading condition. Fatigue crack monitoring was achieved through the use of 20 localized potential drop probes affixed along the length of the weld. Multiple and independent fatigue crack initiation sites were found along the length of the weld. These eventually coalesced and formed a dominant fatigue crack, which led to the eventual failure of the specimens.

Fatigue life estimates using local notch strain and fracture mechanics approaches were obtained. Fatigue crack initiation life estimates using the strain life approach were found to be un-conservative while the estimates of the fatigue crack propagation life were conservative. Accurate knowledge of the structural and weld geometries was found to be critical in the estimation of the fatigue lives.



## **Fatigue Crack Initiation and Growth in A517 SAW Weldments**

**By: Christopher Bayley FTL**

**John Porter DREA**

**May 13 1999**



### **Objectives**

- Effects of Variable Amplitude Load Spectrum on Fatigue Crack Initiation, Propagation and Coalescence
- Generate Experimental data on Fatigue Initiation and Propagation
- Compare Experimental and Numerical Fatigue Crack Predictions

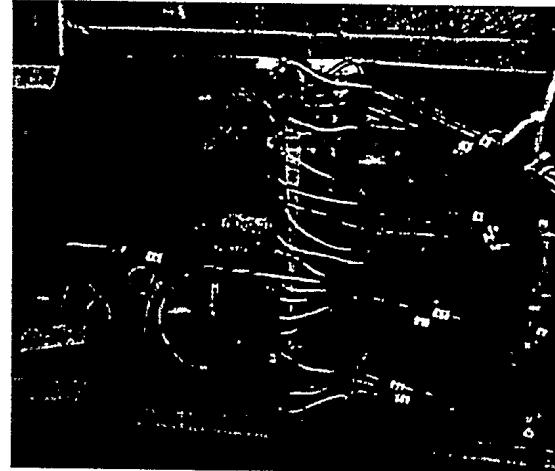
## Experimental Work

### ■ Material Properties

- Cyclic Stress/Strain Curves
- Fatigue Crack Initiation
- Fatigue Crack Growth

### ■ Weld Residual Stresses

### ■ Variable Amplitude Tests on 10" Wide Specimens



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## Material

### ■ 10 mm A517 SAW Material Received from Dockyard Labs

### ■ Representative of the Deck Material used in the Halifax Class Patrol Frigates

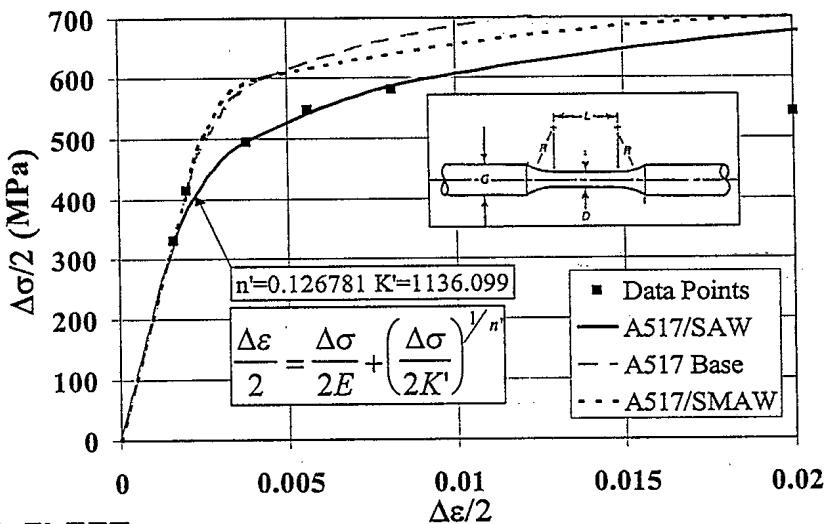
### ■ Samples

- 6 Round Specimens
- 3 Center Crack Panels
- 3 10" Wide Specimens for VA Tests

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## Material Properties

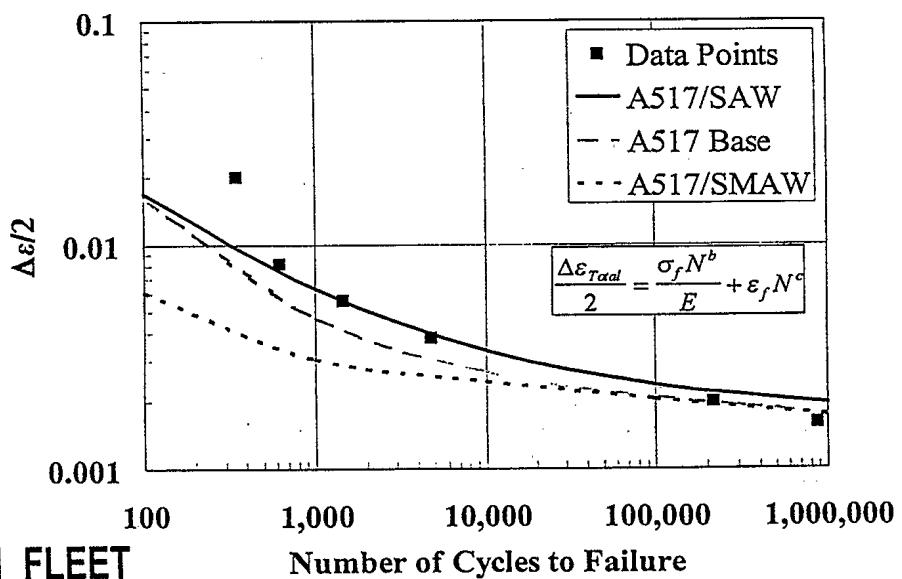
### Cyclic Stress Strain Curve



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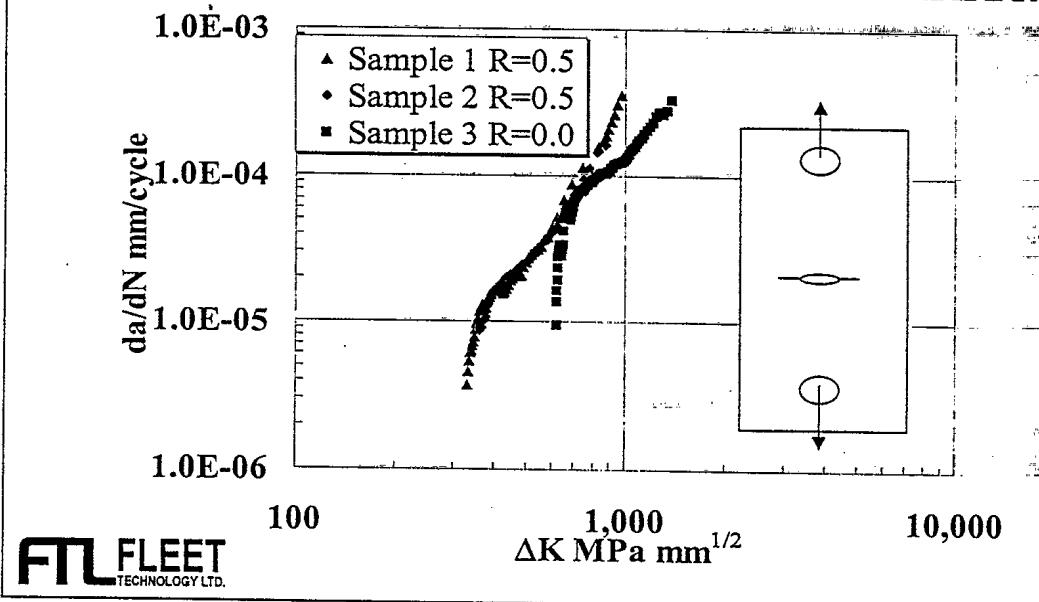
## Material Properties

### Fatigue Crack Initiation



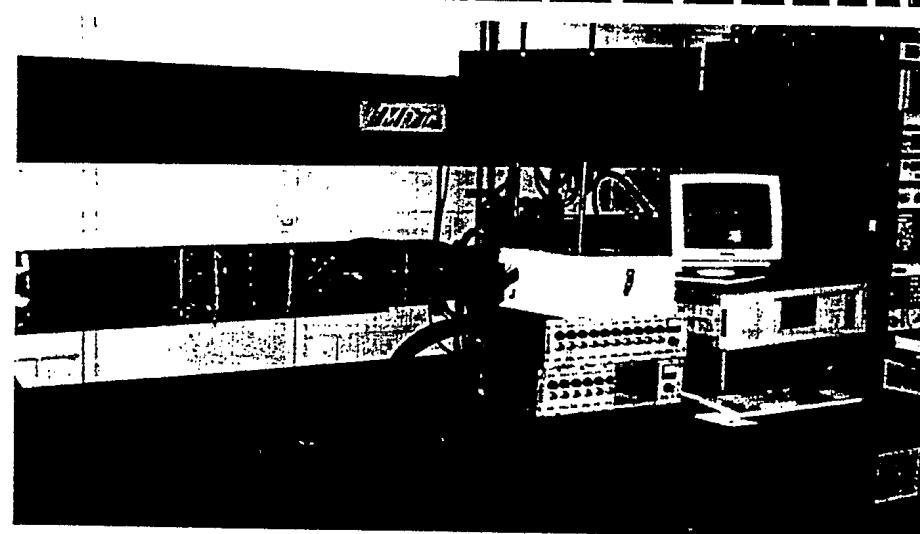
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## Material Properties Fatigue Crack Growth



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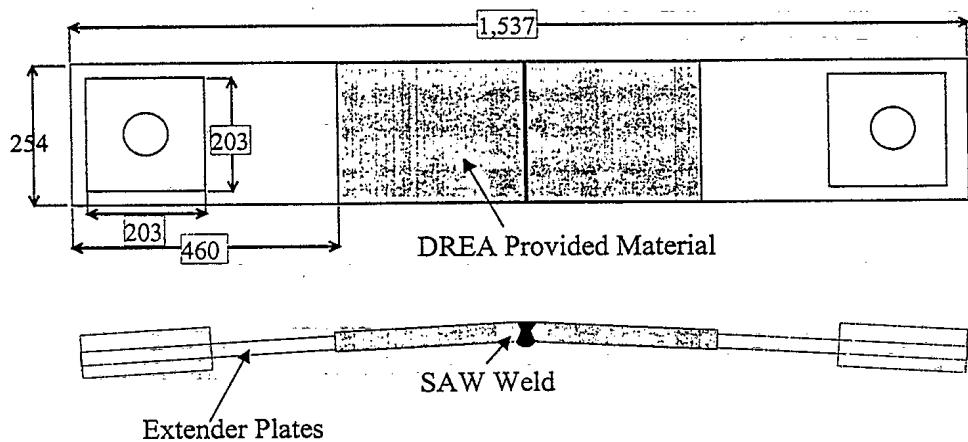
## Variable Amplitude Tests Fatigue Specimens



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## Specimen Characterization

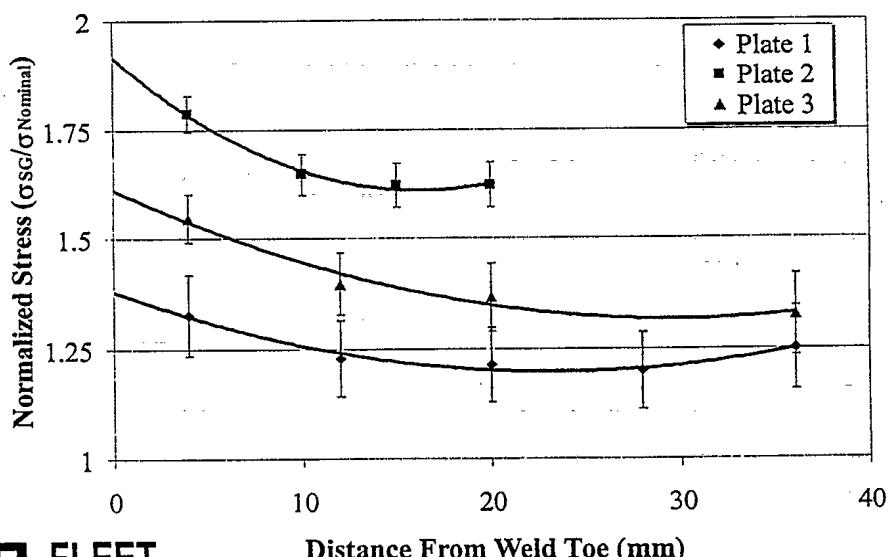
### Specimen Preparation



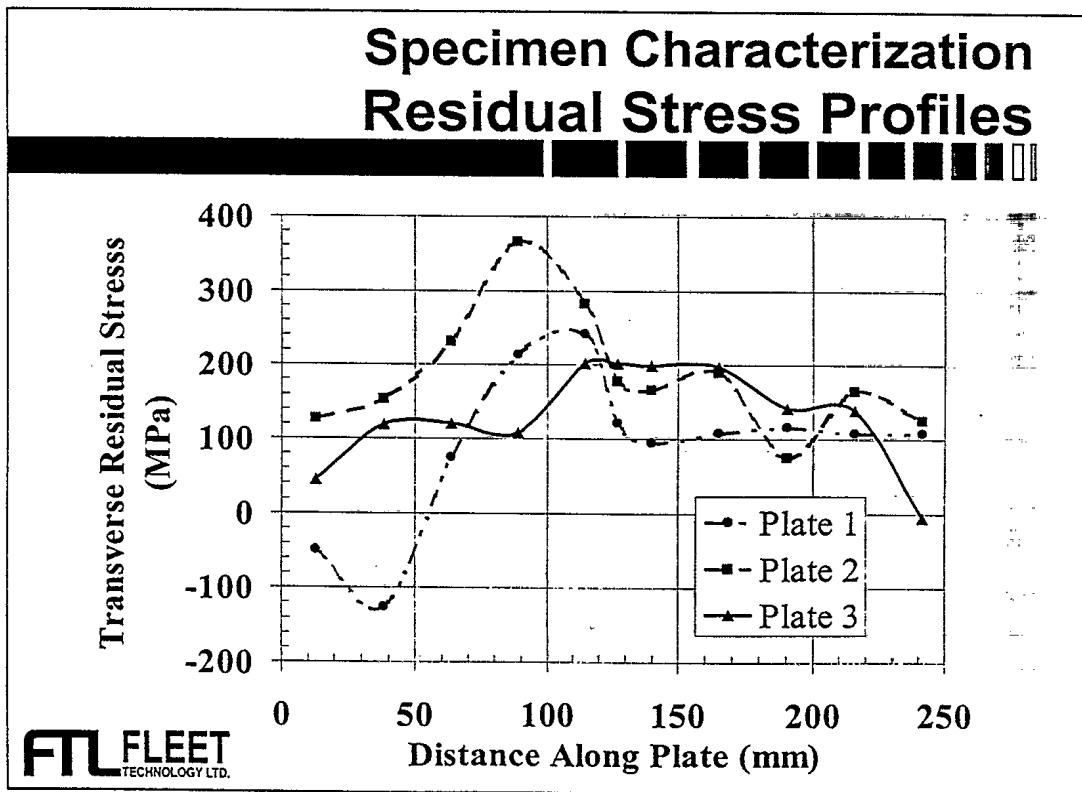
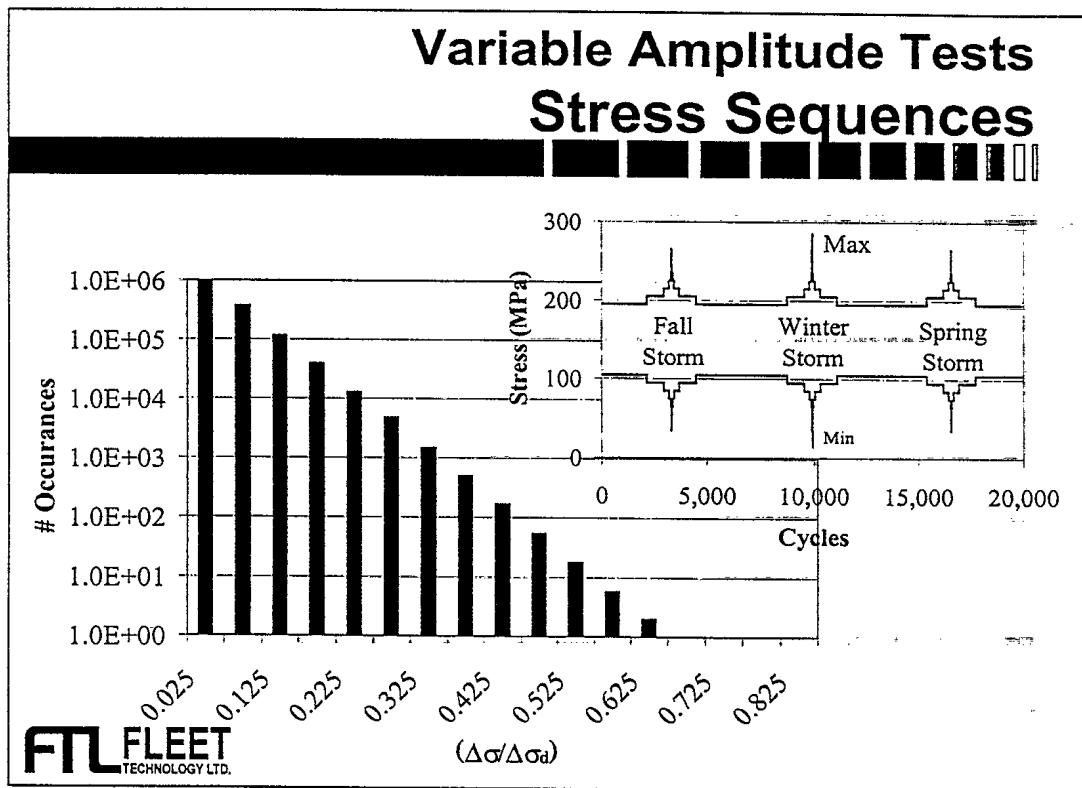
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## Specimen Characterization

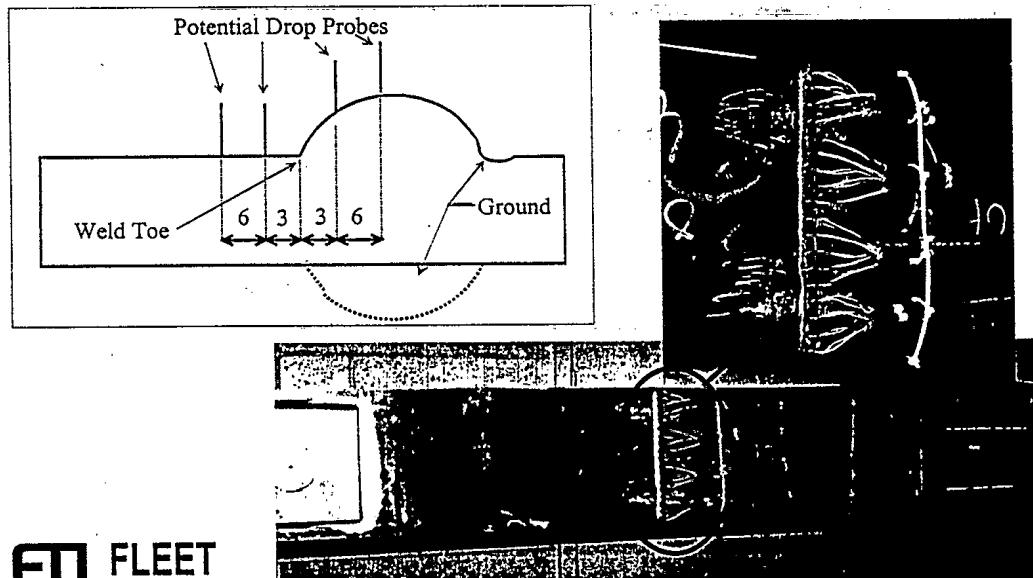
### Hot Spot Stress



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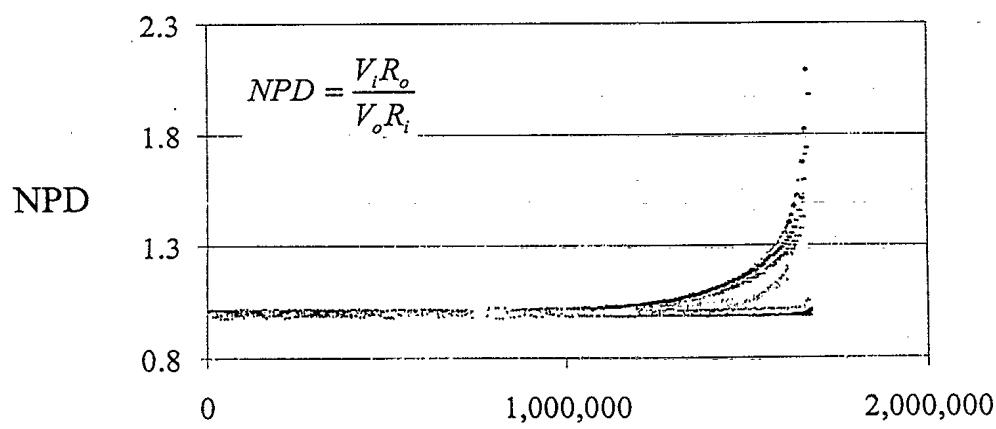


## Variable Amplitude Tests Crack Monitoring



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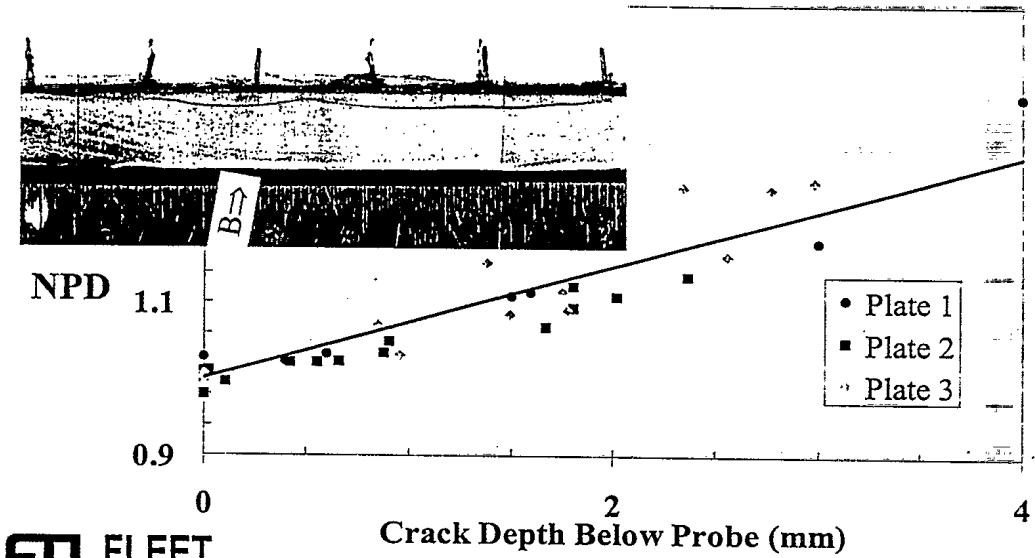
## Variable Amplitude Tests PD Time History



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Cycles

## Variable Amplitude Tests Beachmarks



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## Variable Amplitude Tests Fatigue Crack Initiation Sites

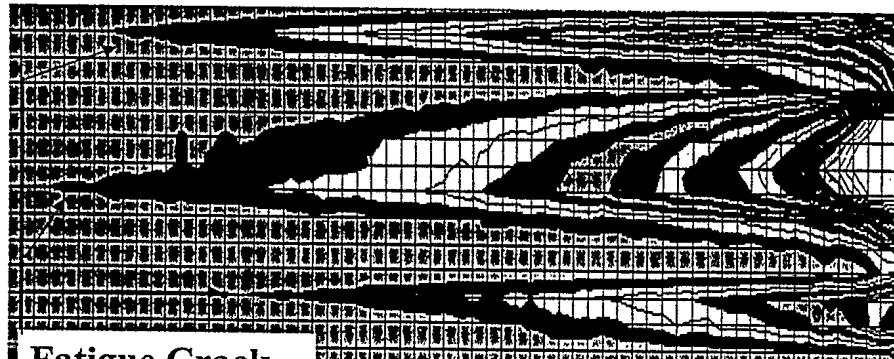
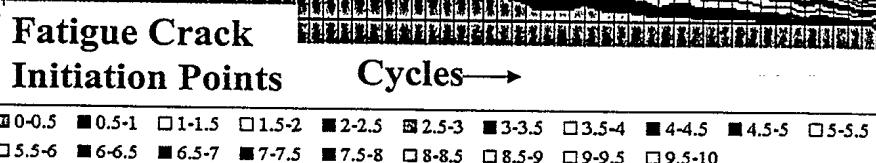


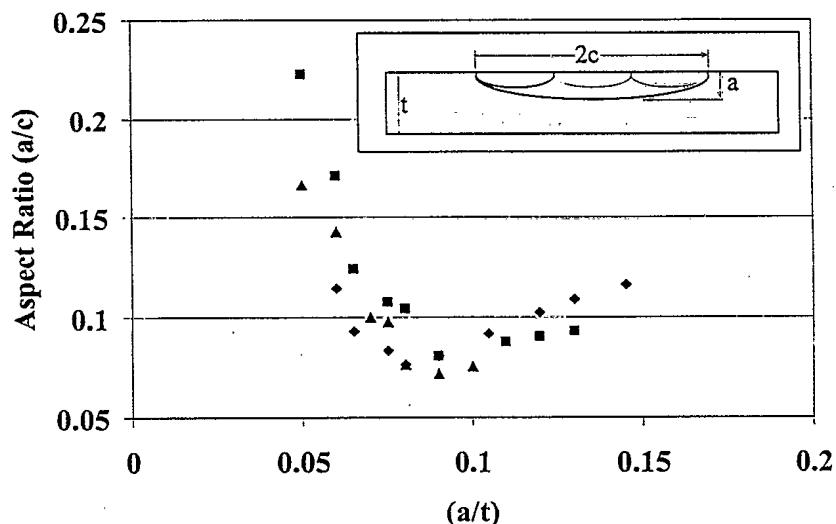
Plate Width (254 mm)



Crack Depth (mm)

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## Variable Amplitude Tests Crack Shape Development



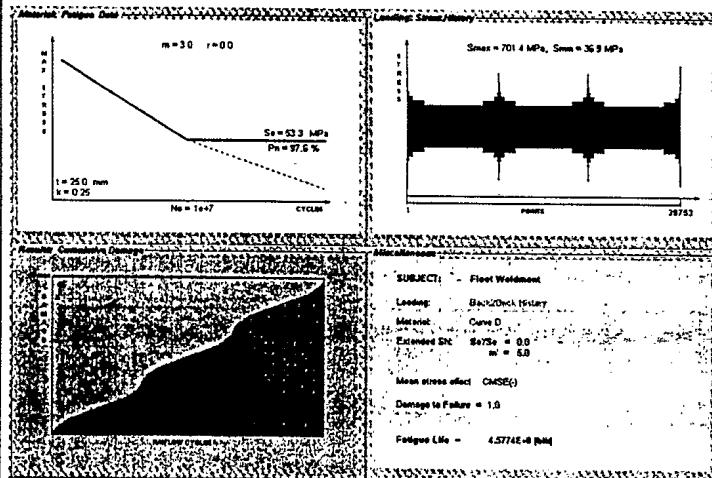
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## Analytical Approach

- Fatigue Crack Initiation and Propagation Software  
FALIN and FALPR
- Work Completed by: Dr Gregory Glinka University of Waterloo, Waterloo Ontario
- Stress Life (SN) Approach
- Strain Life ( $\epsilon N$ ) Approach
- Fatigue Crack Growth ( $da/dN$ )

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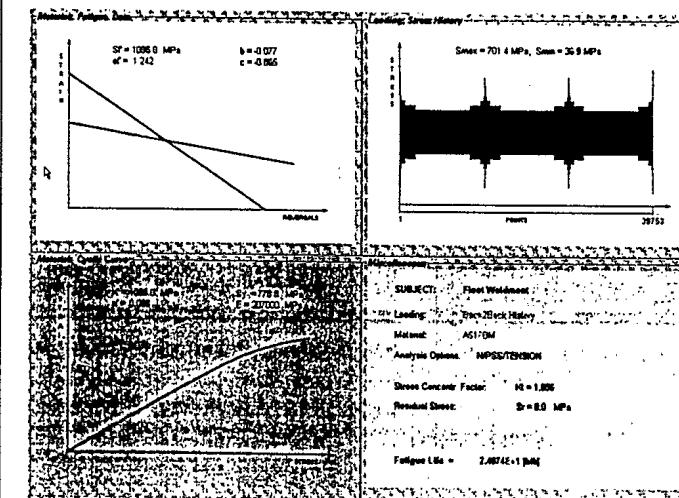
## Analytical Approach Stress Life



- BS-5400 'D' Detail Weld Transverse to Principle Stress dir.
- Miner's Summation used to sum damage from individual cycles
- Significant Damage Caused by Small Stress Ranges

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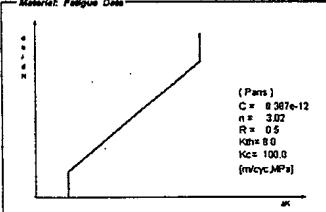
## Analytical Approach Strain Life



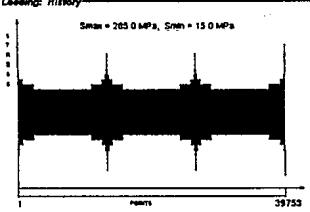
- Local Strain Approach accounts for:
- Geometry of the notch
- Angular Distortion and Straightening of Plates
- Membrane and Bending Components
- Residual Stress State
- Hot Spot Stress

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## Analytical Approach Fatigue Crack Growth

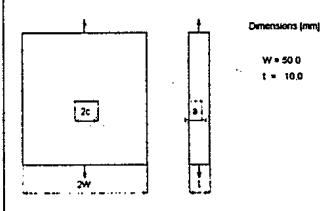
**Material: Fatigue Data**


(Params)  
 $C = 3.307e-12$   
 $n = 3.07$   
 $R = 0.5$   
 $K_{th} = 8.0$   
 $K_c = 100.0$   
 [m/cyc, MPa]

**Loading: History**


$S_{max} = 265.0$  MPa,  $S_{min} = 15.0$  MPa

1 hours 39753

**Geometry: Crack Case**


Dimensions [mm]  
 $W = 50.0$   
 $t = 10.0$

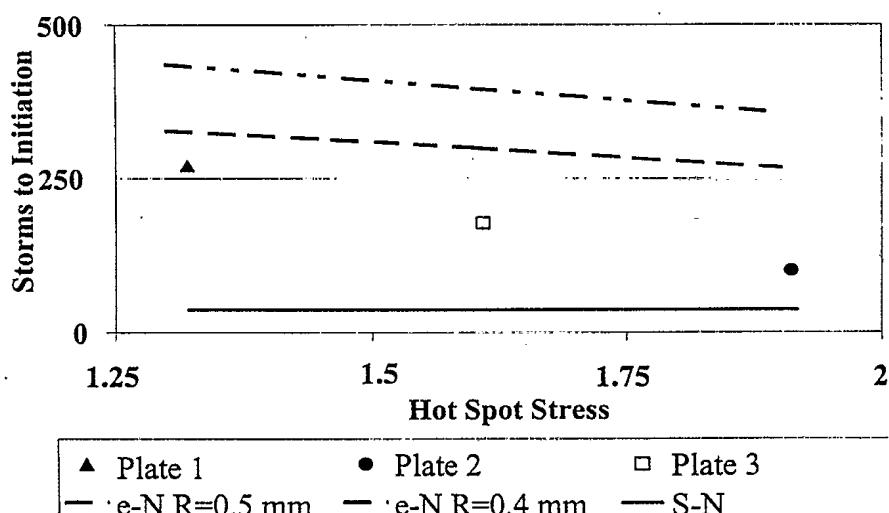
**Miscellaneous**

Subject	Case6	
Loading	Back2Back History	
Material	AS17	
Crack Loading	FleetSW	
Analysis Option	RNF/C-CR/H	
Initial Crack $a$ [mm]	0.25	a/c = 1.0
Final Crack $a$ [mm]	5.906 (DF)	a/c = 0.428
Fatigue life	$7.38000e+0$ [h] 180000 cyc.	

- Fatigue Crack Growth based on SIF and cycle by cycle integration
- Local Geometry affects included in SIF
- Model includes Variation in Membrane and Bending Stress
- FCR of a Single Semi-Elliptical Flaw

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## Results Experimental & Numerical

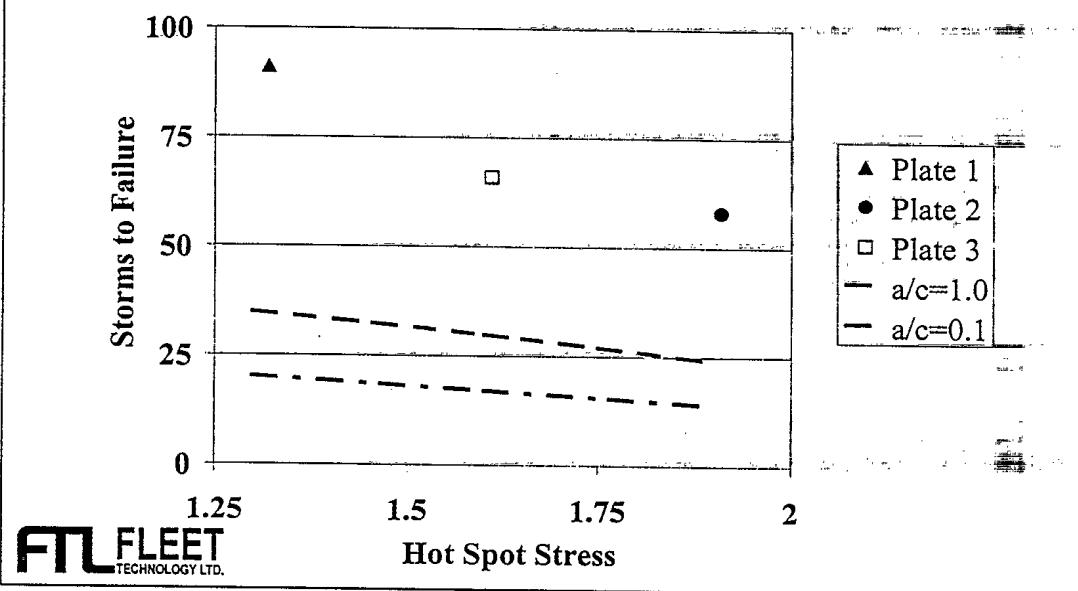


Hot Spot Stress	Plate 1 (e-N R=0.5 mm)	Plate 1 (e-N R=0.4 mm)	Plate 2 (e-N R=0.5 mm)	Plate 2 (e-N R=0.4 mm)	Plate 3 (e-N R=0.5 mm)	Plate 3 (e-N R=0.4 mm)	S-N (cycles)
1.25	250	250	250	250	250	250	100
1.5	280	280	280	280	280	280	100
1.75	300	300	300	300	300	300	100
2.0	320	320	320	320	320	320	100

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## Results

### Experimental & Numerical



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## Conclusions

### Numerical

- S-N VERY Conservative
- $\varepsilon$ -N Over-Predicts Fatigue Initiation
  - Requires detailed information specific to each geometry
- Fatigue Crack Growth
  - Conservative if omit Retardation effects

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## Conclusions Experimental



- Fatigue Crack Initiation accounts for 70% of Total Fatigue Life
- Variable Amplitude Loading affects the Number of Initiation Sites
- Fatigue Life Affected by:
  - Hot Spot Stress Concentration
  - Notch Geometry
  - Angular Distortion of Specimens
  - Load Spectrum



## Recommendations Future Research



- Determine the influence of weld shape and residual strains on the fatigue performance of butt welded joints
- Variable and Constant Amplitude Tests
- Weld Toe Improvements and Fatigue Life
- Examine Agreement between Numerical Predictions and Experimental tests

